

Anisotropy migration of self-point defects in dislocation stress fields in BCC Fe and FCC Cu

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Abstract

Spatial dependence of the interaction energies of self-point defects (vacancies and self interstitial atoms in stable, meta-stable and saddle point configurations) with edge dislocations in slip systems $\langle 111 \rangle \{110\}$ and $\langle 100 \rangle \{100\}$ in BCC Fe and $\langle 110 \rangle \{111\}$ in FCC Cu was calculated using the anisotropic theory of elasticity and molecular statics (hybrid method). The migration pathways of vacancies and SIA ($\langle 110 \rangle$ dumbbell in Fe and $\langle 100 \rangle$ dumbbell in Cu) along which the migration of the defects with the lowest energy barriers were defined in the presence of the dislocation stress fields. These pathways are significantly different in the stress fields of dislocations.

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1. Introduction

Stress fields of dislocations, the basic source of internal stresses, considerably effect the kinetic behavior of point defects including their diffusion and absorption by dislocations as sinks. Such processes depend on the symmetry of crystal lattices, elastic anisotropy of crystals and types of crystal defects [1]. It is important to study the influence of dislocation stress fields on formation and migration energies of vacancies and self interstitial atoms (SIA) in crystals of different crystallographic classes.

Here, the spatial dependence of the elastic interaction energy between the self-point defects (SPDs) in stable, metastable and saddle point configurations and straight edge dislocations with different

Burgers vectors in BCC Fe and FCC Cu were calculated using a hybrid method. Elastic fields of dislocations and their interactions with SPDs (elastic dipoles) were calculated in the framework of the anisotropic theory of elasticity [2]. Characteristics of SPDs (formation and migration energies, relaxation volumes and dipole moment tensors) in the absence of stress fields were calculated by molecular statics. The influence of these interactions on the migration directions of the SPDs was studied to understand their influence on radiation-induced property changes such as swelling in crystals with different symmetries (BCC, FCC).

2. SPDs characteristics

Formation energies E^F , relaxation volumes V^R , and dipole tensors P_{ij} ($i, j = 1, 2, 3$, define the coordinate axes in crystallographic coordinate system) of

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SPDs in stable, metastable and saddle point configurations were calculated in [3,4]. Interatomic interactions in model crystallites were described by an interaction potential from [5] for BCC Fe and by EAM-type interaction potential from [6] for FCC Cu. Table 1 lists calculated characteristics of SPDs in Fe and Cu. Comparison of the characteristics of SPDs presented here in the absence of the stresses with experimental data was conducted in [3,6] and demonstrated good agreement.

The stable SIA configurations are the $\langle 110 \rangle$ dumbbell in Fe and the $\langle 100 \rangle$ dumbbell in Cu. The $\langle 110 \rangle$ and $\langle 100 \rangle$ dumbbells jump to the nearest lattice sites with a 60° and 90° rotation of the dumbbell axis, respectively. This is the SIA migration mechanism with the lowest migration energy, 0.25 eV and 0.10 eV, in Fe and Cu. The elastic dipole corresponding to the saddle point configuration of the $\langle 110 \rangle$ and $\langle 100 \rangle$ dumbbells has 12 (monoclinic symmetry) and 6 (orthorhombic symmetry) possible equivalent orientations, respectively (Table 1).

The elastic dipole corresponding to the vacancy saddle point configuration has four possible equivalent orientations (trigonal symmetry) in Fe and six (orthorhombic symmetry) in Cu (Table 1). The vacancy migration energy is equal to 0.735 eV and 0.69 eV in Fe and Cu, respectively.

3. Elastic stress fields of dislocations

Stress fields, σ_{ij}^d , of straight perfect edge dislocations in slip systems $\langle 111 \rangle \{110\}$ (Burgers vector $\mathbf{b} = a/2[111]$) and $\langle 100 \rangle \{100\}$ ($\mathbf{b} = a[100]$) in Fe and $\langle 110 \rangle \{111\}$ ($\mathbf{b} = a/2[110]$) in Cu were calculated within the anisotropic linear theory of elasticity, following an algebraic method [2]. Elastic constants C_{11} , C_{12} , C_{44} and lattice constants a used for calculation of dislocation stress fields are in accord with values provided the interatomic potential used: $C_{11} = 243.1$ GPa, $C_{12} = 138.1$ GPa, $C_{44} = 121.9$ GPa, $a = 0.28665$ nm for Fe; $C_{11} = 169.9$ GPa, $C_{12} = 122.6$ GPa, $C_{44} = 76.2$ GPa, $a = 0.3615$ nm for Cu.

4. Interaction of dislocations with SPDs

The formation energy E_d^F of a point defect in the neighborhood of a dislocation can be written as

$$E_d^F(\mathbf{r}) = E^F + E_{\text{int}}(\mathbf{r}), \quad (1)$$

where E^F is the formation energy of the point defect in the absence of the dislocation, \mathbf{r} is the radius-vector of the position of the point defect with respect to the dislocation and E_{int} is the interaction energy between the dislocation and the point defect.

Table 1

Calculated formation energies E^F (in eV), relaxation volumes V^R (in atomic volumes) and dipole tensors P_{ij} (in eV) of self-point defects in BCC Fe and FCC Cu in the absence of dislocation stress fields (N is the number of possible crystallographic orientations for the considered elastic dipoles) [3,4]

Material	Self-point defect	E^F ^a	V^R	P_{11}	P_{22}	P_{33}	P_{13}	P_{23}	P_{12}	N^b
Fe	$\langle 110 \rangle$ dumbbell	4.384	1.480	18.04	18.04	20.39	0	0	4.99	6
	$\langle 110 \rangle$ dumbbell saddle point	4.630	1.476	18.88	18.57	18.88	3.26	5.16	5.16	12
	$\langle 111 \rangle$ dumbbell	4.627	1.436	18.27	18.27	18.27	6.37	6.37	6.37	4
	Crowdion	4.635	1.442	18.35	18.35	18.35	6.32	6.32	6.32	4
	Tetrahedral	5.149	1.286	15.60	16.74	16.74	0	0	0	3
	Octahedral	5.464	1.174	21.02	11.89	11.89	0	0	0	3
	$\langle 100 \rangle$ dumbbell	5.618	1.171	19.86	12.41	12.41	0	0	0	3
	Vacancy	1.920	-0.140	-1.78	-1.78	-1.78	0	0	0	1
	Vacancy saddle point	2.655	-0.112	-1.43	-1.43	-1.43	-1.68	-1.68	-1.68	4
	Cu	$\langle 100 \rangle$ dumbbell	3.068	1.848	18.55	18.99	18.99	0	0	0
$\langle 100 \rangle$ dumbbell saddle point		3.166	1.887	19.09	19.09	19.57	0	0	2.22	6
Octahedral		3.243	1.902	19.40	19.40	19.40	0	0	0	1
$\langle 110 \rangle$ dumbbell		3.302	1.906	18.38	18.38	21.57	0	0	10.48	6
Crowdion		3.303	1.904	18.36	18.36	21.55	0	0	10.46	6
$\langle 111 \rangle$ dumbbell		3.504	1.945	19.84	19.84	19.84	3.53	3.53	3.53	4
Tetrahedral		3.553	1.959	19.98	19.98	19.98	0	0	0	1
Vacancy		1.272	-0.298	-3.04	-3.04	-3.04	0	0	0	1
Vacancy saddle point		1.962	-0.189	-3.72	-3.72	1.66	0	0	-0.76	6

^a The values of the self-point defect formation energies presented in Table 2 of [5] are incorrect.

^b $N = 1, 3, 4, 6, 12$ corresponds to cubic, tetragonal, trigonal, orthorhombic, monoclinic symmetries of point defect configuration, respectively.

The interaction energy E_{int} within the framework of the linear theory of elasticity is given by [1,7–9]

$$E_{\text{int}}(\mathbf{r}) = E_{\text{int}}(r, \varphi) = -P_{ij} \varepsilon_{ij}^{\text{d}}(\mathbf{r}) \\ = -P_{ij} S_{ijkl} \sigma_{kl}^{\text{d}}(\mathbf{r}), \quad (2)$$

where r is the distance between the point defect (elastic dipole) and the dislocation, φ is the angle between \mathbf{r} and \mathbf{b} , S_{ijkl} is the elastic compliance tensor and $\varepsilon_{ij}^{\text{d}}$ is the elastic strain tensor caused by a dislocation. At distances less than $\sim a$, it is necessary to use additionally atomistic models ([3,10,11]) to check the validity of the linear approximation.

Dislocation stress fields eliminate degeneracy of the formation energies of crystallographically equivalent different orientations of SPDs. This can result in: (1) change of the most energetically favorable SIA configuration near the dislocation, and (2) anisotropic migration of SPDs.

4.1. Change of stable SIA configuration in the neighborhood of dislocations

Near a $\langle 111 \rangle \{110\}$ dislocation in Fe, the formation energy of a $\langle 111 \rangle$ dumbbell is less than the formation energy of a $\langle 110 \rangle$ dumbbell. Fig. 1(a) shows the region of stabilization of a $\langle 111 \rangle$ dumbbell and spatial dependence of the most energetically favorable $\langle 111 \rangle$ dumbbell orientations. In the angle range $7^\circ < \varphi < 173^\circ$, the most energetically prefera-

ble SIA configuration is a $\langle 111 \rangle$ dumbbell with the axis parallel to the Burgers vector orientation. The $\langle 111 \rangle$ dumbbell formation energy maximum at $\varphi = 90^\circ$ is located between two minimums at angles of $\varphi = 70^\circ$ and $\varphi = 110^\circ$. In the specified angle range, a $\langle 111 \rangle$ dumbbell has to change its orientation to the energetically unfavourable one to get closer to the dislocation. Therefore, $\langle 111 \rangle \{110\}$ dislocation stress fields make a field-effect trap for $\langle 111 \rangle$ dumbbell, which makes its approach to the dislocation core difficult. This result is in agreement with the results of the molecular dynamics study [12]. The stabilization region of a $\langle 111 \rangle$ dumbbell is absent in the neighborhood of a $\langle 100 \rangle \{100\}$ dislocation in Fe.

In the neighborhood of a $\langle 110 \rangle \{111\}$ dislocation in Cu, the formation energy of a $\langle 110 \rangle$ dumbbell is less than the formation energy of a $\langle 100 \rangle$ dumbbell. Fig. 1(b) shows the region of stabilization of a $\langle 110 \rangle$ dumbbell and the spatial dependence of the most energetically favorable $\langle 110 \rangle$ dumbbell orientations. In the angle ranges $-11^\circ < \varphi < 82^\circ$ and $98^\circ < \varphi < 191^\circ$ the most energetically preferable SIA configuration is a $\langle 110 \rangle$ dumbbell with the axis parallel to the slip plane orientation. $\langle 110 \rangle$ dumbbell formation energy minimums are located at angles $\varphi = 40^\circ$ and $\varphi = 140^\circ$. In the specified angle ranges, a $\langle 110 \rangle$ dumbbell has to change its orientation to the energetically unfavourable one to get closer to the dislocation core. Therefore, $\langle 111 \rangle \{110\}$ dislocation

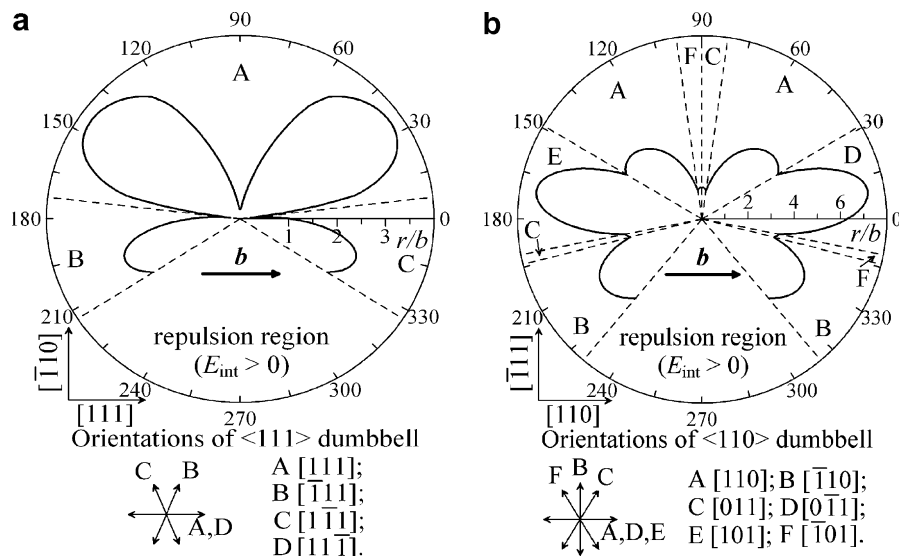


Fig. 1. Spatial regions of stabilization for SIA configurations in the neighborhood of dislocations (dotted lines demarcate the regions with different energetically favorable orientations of the self interstitial). (a) $\langle 111 \rangle$ dumbbell, $\langle 111 \rangle \{110\}$ dislocation, Fe; (b) $\langle 110 \rangle$ dumbbell, $\langle 110 \rangle \{111\}$ dislocation, Cu.

stress fields make a field-effect trap for $\langle 110 \rangle$ dumbbell, which makes its approach to the dislocation core difficult. However, in the angle range $82^\circ < \varphi < 98^\circ$ the most energetically preferable $\langle 110 \rangle$ dumbbell orientations are directed toward the dislocation core.

4.2. Migration of SPDs in the neighborhood of dislocations

Each orientation of an elastic dipole relative to a point defect saddle point configuration corresponds to a certain migration direction. Using Eqs. (1) and (2) to calculate the formation energies of all possible orientations of the defect saddle point configuration at some point r , we can determine the point defect migration direction with the lowest migration energy at this point and plot migration pathways along which the migration of the point defect has the lowest energy barriers.

To characterize distances at which anisotropic migration becomes significant, we calculated average distances \bar{r} (Table 2) to the dislocations, at which difference between migration energies of the SPDs in different directions is larger than value of $k_B T$ (k_B is Boltzmann's constant) at $T = 293$ K. \bar{r} for SIA is three times as large as \bar{r} for vacancy in Fe. However, \bar{r} for SIA is half as large as \bar{r} for vacancy in Cu. These features are the consequence of highly anisotropic dipole tensors for saddle point configurations of the $\langle 110 \rangle$ dumbbell in Fe and vacancy in Cu and relatively low anisotropy for saddle point configurations of the $\langle 100 \rangle$ dumbbell in Cu and vacancy in Fe (Table 1).

4.2.1. $\langle 111 \rangle \{110\}$ dislocation in Fe

For the $\langle 110 \rangle$ dumbbell attractive region, the pathways are parallel to the slip plane, which makes it difficult for the SIA to approach the dislocation (Fig. 2(a)). Besides, in the neighborhood of the dislocation, the SIA falls into the field-effect trap mentioned above.

Table 2

Average distance \bar{r} to the dislocations, at which difference between migration energies of the self-point defects in different directions is larger than the value of $k_B T$ at $T = 293$ K

Material	Dislocation	\bar{r} (b)	
		SIA	Vacancy
Fe	$\langle 111 \rangle \{110\}$	60	19
	$\langle 100 \rangle \{001\}$	30	9
Cu	$\langle 110 \rangle \{111\}$	16	28

In the vacancy attractive region in the angle range $233^\circ < \varphi < 307^\circ$, the migration directions with the lowest migration energy are parallel to the Burgers vector and directed outwards from the dislocation which makes it difficult for it to approach the dislocation (Fig. 2(b)).

4.2.2. $\langle 100 \rangle \{100\}$ dislocation in Fe

In the angle range $-39^\circ < \varphi < 219^\circ$ (Fig. 2(c)), the migration directions of a $\langle 110 \rangle$ dumbbell with the lowest migration energy are directed towards the dislocation. The stabilization region of a $\langle 111 \rangle$ dumbbell is absent, so the SIA can fall into the dislocation core without difficulties.

In the angle range $260^\circ < \varphi < 280^\circ$ (Fig. 2(d)), the migration directions of a vacancy with the lowest migration energy are directed outwards from the dislocation which makes it difficult for it to approach the dislocation.

4.2.3. $\langle 110 \rangle \{111\}$ dislocation in Cu

In the $\langle 100 \rangle$ dumbbell attraction region, the pathways are parallel to the dislocation slip plane with the exception of the angle range $82^\circ < \varphi < 98^\circ$ (Fig. 2(e)). In this region the migration directions of a $\langle 100 \rangle$ dumbbell with the lowest migration energies are directed to the dislocation. Thus, the pathways of an SIA with the lowest energy barriers move around the field-effect trap mentioned above because of the change of the most stable SIA configuration near the dislocation.

In the angle ranges $218^\circ < \varphi < 245^\circ$, $262^\circ < \varphi < 278^\circ$, $295^\circ < \varphi < 322^\circ$ (Fig. 2(f)), the migration directions of a vacancy with the lowest migration energy are directed outwards from the dislocation which makes it difficult for it to approach the dislocation.

5. Conclusion

1. Interaction energies of SPDs (elastic dipoles) with edge dislocations in slip systems $\langle 111 \rangle \{110\}$ and $\langle 100 \rangle \{100\}$ in BCC Fe and $\langle 110 \rangle \{111\}$ in FCC Cu were calculated by methods of the anisotropic theory of elasticity and molecular statics (hybrid method).
2. Crystallographic characteristics of SPDs and edge dislocations significantly effect the migration energies of SPDs in dislocation stress fields.
3. $\langle 110 \rangle$ dumbbell jumps with the lowest migration energy are directed parallel to the Burgers vector in the attractive region of an SIA with a $\langle 111 \rangle \{110\}$ dislocation in Fe. Dislocation stress

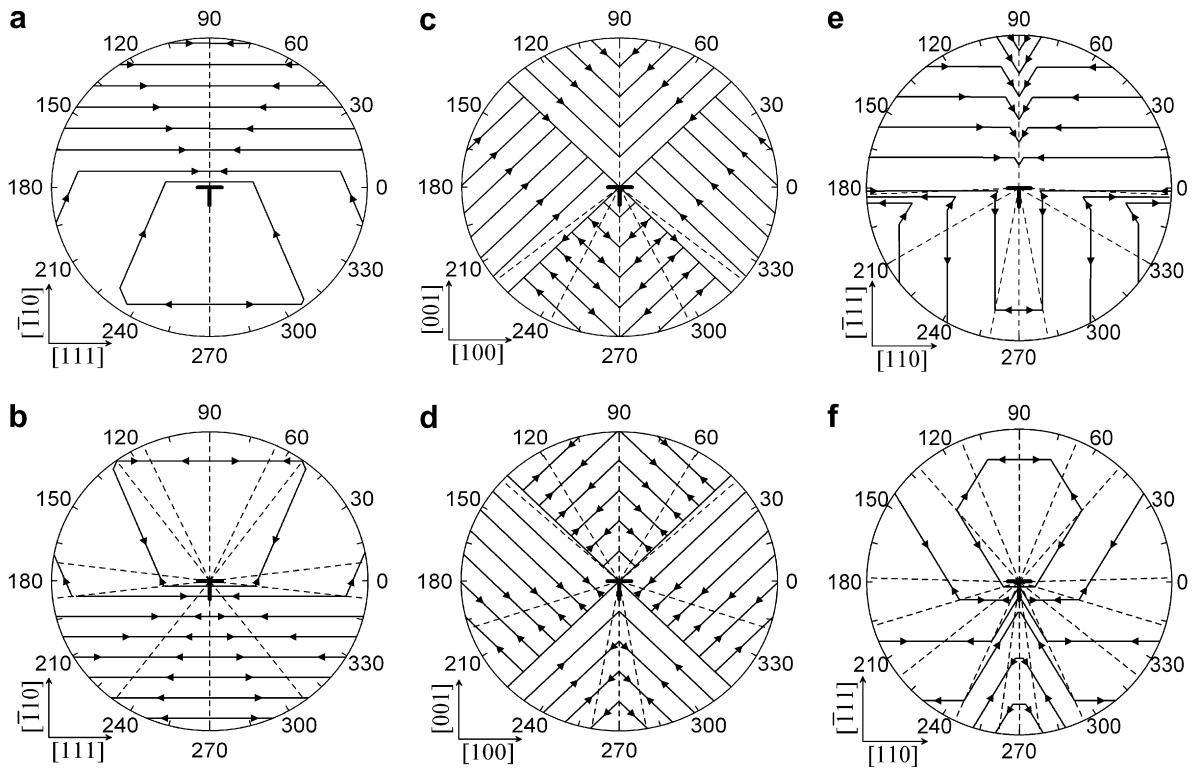


Fig. 2. Migration pathways of the self-point defects with the lowest energy barriers in dislocation stress fields (arrows show the direction of the self-point defect motion along the pathway; dotted lines are rays $\varphi = \text{const.}$ corresponding to turning points in the defect migration along the pathway). (a) $\langle 110 \rangle$ dumbbell, $\langle 111 \rangle \{110\}$ dislocation, Fe; (b) vacancy, $\langle 111 \rangle \{110\}$ dislocation, Fe; (c) $\langle 110 \rangle$ dumbbell, $\langle 100 \rangle \{100\}$ dislocation, Fe; (d) vacancy, $\langle 100 \rangle \{100\}$ dislocation, Fe; (e) $\langle 100 \rangle$ dumbbell, $\langle 110 \rangle \{111\}$ dislocation, Cu; (f) vacancy, $\langle 110 \rangle \{111\}$ dislocation, Cu.

fields stabilize the $\langle 111 \rangle$ dumbbell configuration of an SIA oriented parallel to the Burgers vector, which also impedes SIA approach to the dislocation.

4. In the neighbourhood of $\langle 100 \rangle \{100\}$ dislocation in Fe, the region of stabilization of the $\langle 111 \rangle$ dumbbell is absent, and the migration directions of a $\langle 110 \rangle$ dumbbell with the lowest migration energy are directed towards the dislocation.
5. A $\langle 100 \rangle$ dumbbell can migrate to the $\langle 110 \rangle \{111\}$ dislocation core in Cu without difficulties since the pathways of an SIA with the lowest energy barriers move around the field-effect trap concerned with the stabilization of a $\langle 110 \rangle$ dumbbell oriented parallel to the Burgers vector near the dislocation.
6. Vacancy migration to the considered dislocations is impeded since the migration directions of a vacancy with the lowest migration energy are directed outwards from the dislocation.
7. Average distance to the dislocations, at which difference between migration energies of the

SPDs in different directions is larger than value of $k_B T$ at $T = 293$ K, equals $\sim 30b$ and may significantly vary depending on the dislocation type and SPD configuration.

8. Indicated features of SPDs behavior in dislocation fields can exert a significant influence on the efficiency of the dislocations as sinks for SPDs in crystals with different symmetries and, consequently, on evolution of material microstructure under damage irradiation (swelling, creep, etc).

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